



Thermal Management Systems Symposium

October 14-15, 2025 Ypsilanti, Michigan

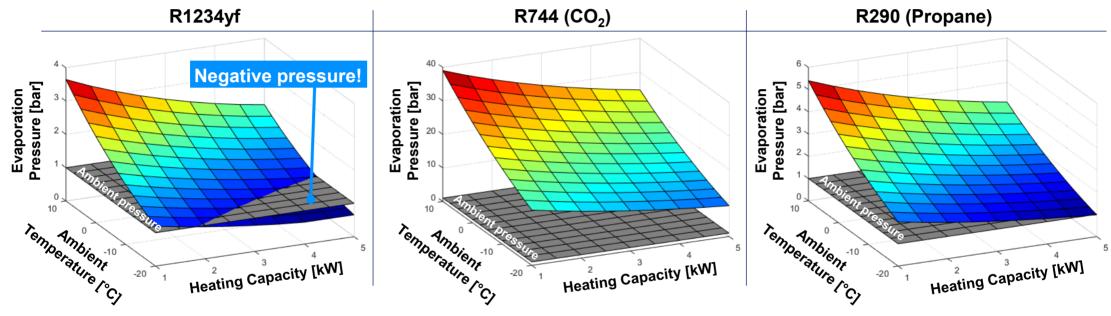
Comparing RAFT PUBLICATION OF R290 Refrigerar FOR Estems for Electric Vehicles

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Motivation

- The investigation and development of R290 refrigerant cycles are a major focus for many OEMs and suppliers.
- Main reasons: PFAS regulations, heat pump usage even at low temperatures, cost pressure for system and components



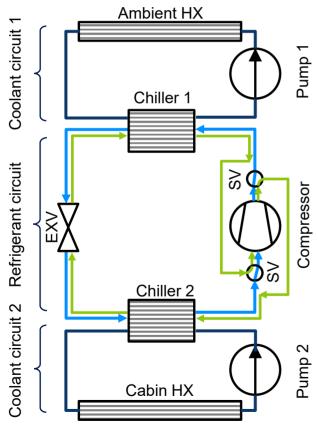
- Widely used refrigerant, but PFAS!
- Limitations already at temperatures below -5 °C
 - **→** PTC-Heater or other technical solutions required
- favored refrigerant for very low temperatures
- very high system pressure (> 100 bar)
 - → requires specially designed components (high costs)

- suitable for significantly lower temperatures than R1234yf
- only slightly higher pressures
- Highly flammable
 - **→** safety concept required!

Hint: if evaporation pressure < ambient pressure → negative pressure in the system → tightness cannot be guaranteed → negative pressure must be avoided!

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- Due to safety concerns, there is a trend towards designing R290 circuits as fully indirect systems
- Simplified circuit:



Advantages:

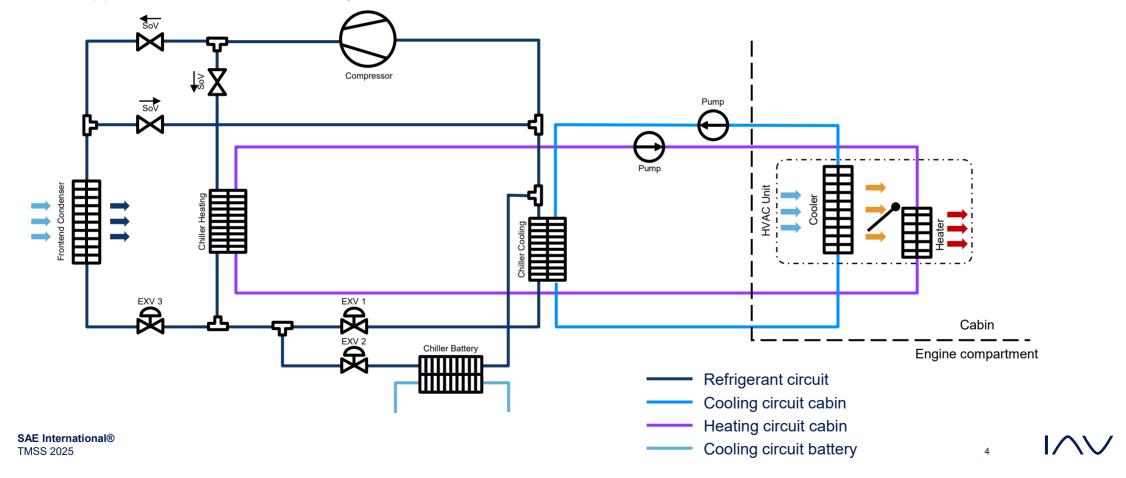
- very compact refrigerant circuit → low refrigerant charge
- Compact system might be filled and tested by the supplier
 → no flammable refrigerant at the OEM final assembly line

Disadvantages:

- More complex water side, especially for heat pump mode
- Lots of water pumps and valves
- high system inertia due to the coolant circuits
- critical in terms of installation space and costs
 - → compact system might be difficult to package

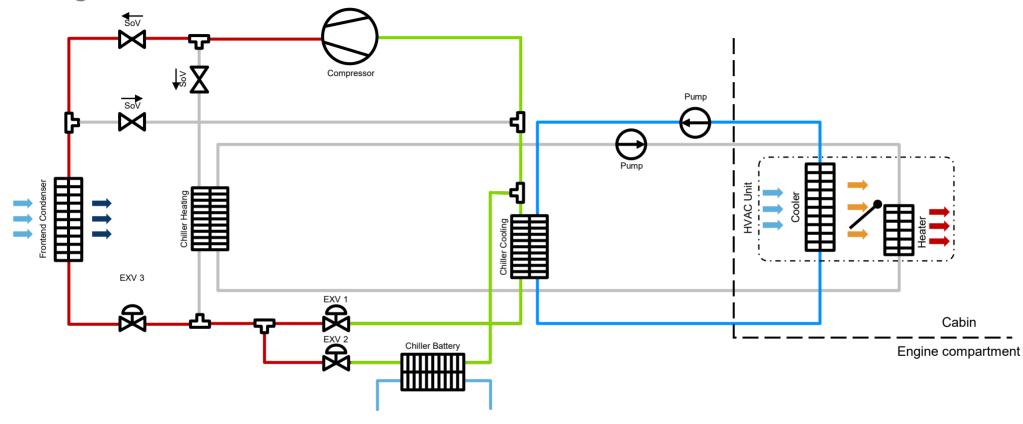
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- IAV approach: Semi-Direct R290 system



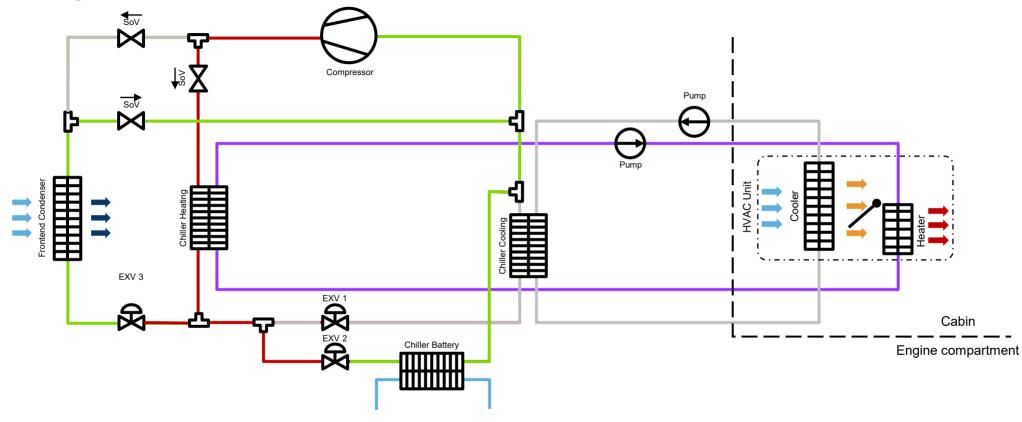
Semi-Direct R290 system

Cooling mode



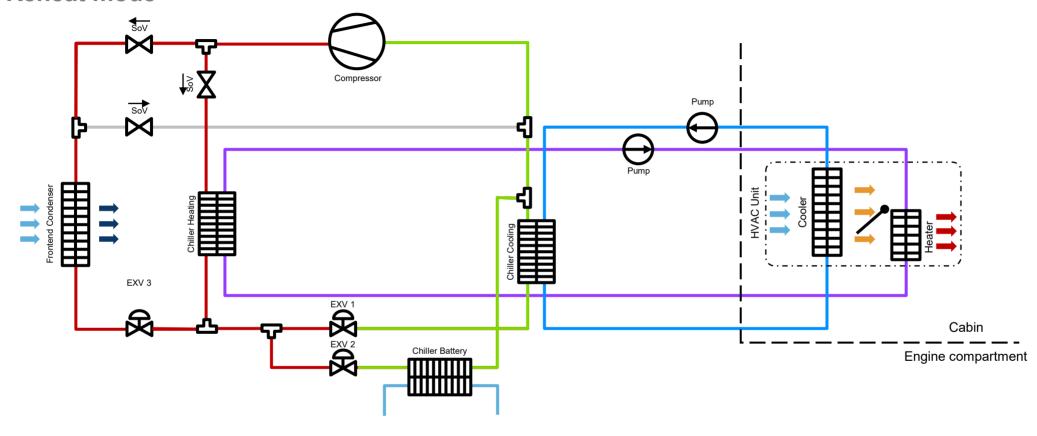
Semi-Direct R290 system

Heating mode



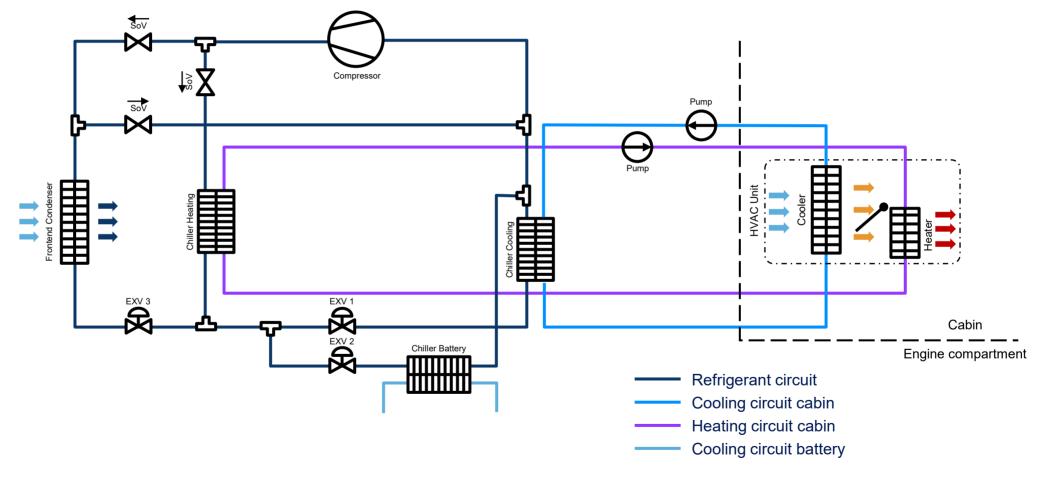
Semi-Direct R290 system

Reheat mode



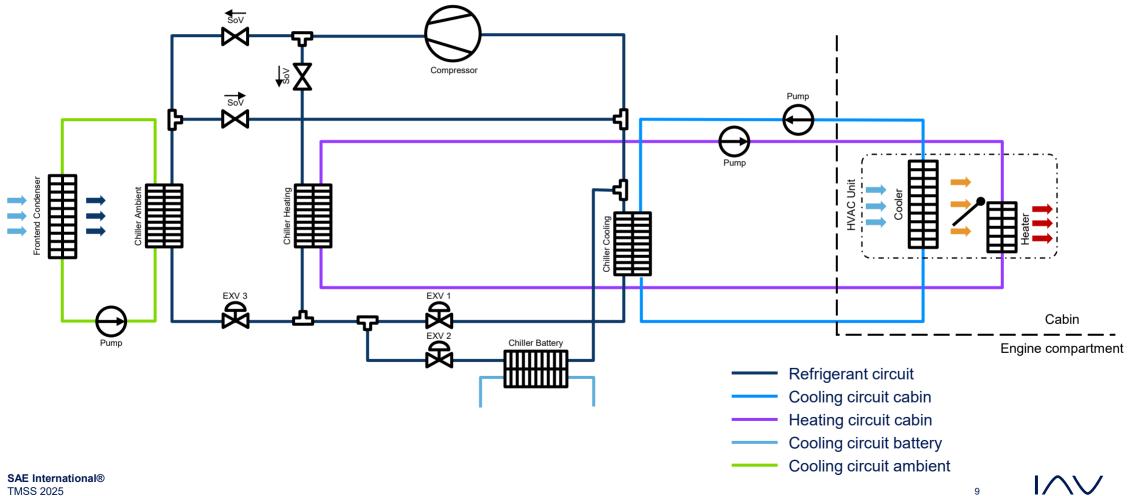
Investigation goals

Comparison of the Semi-Direct System with a fully indirect system (and a direct system)



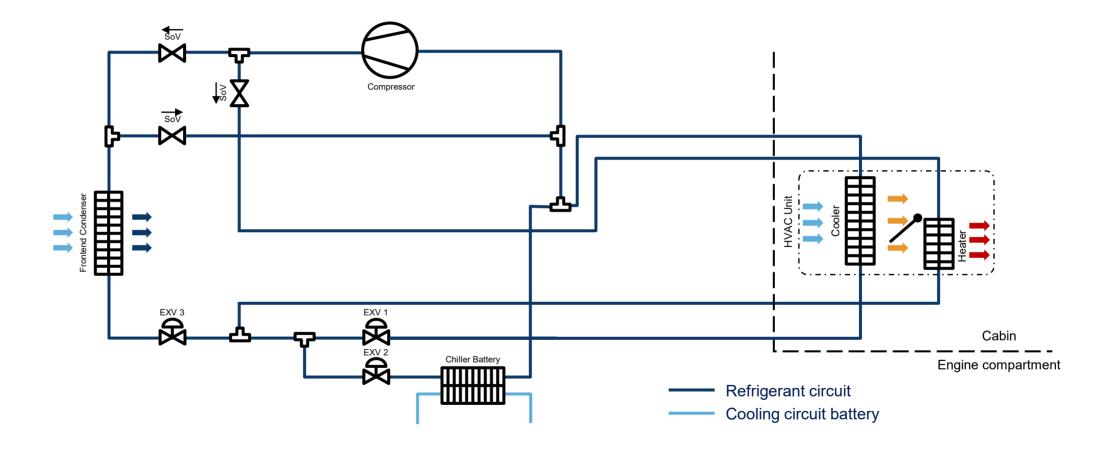
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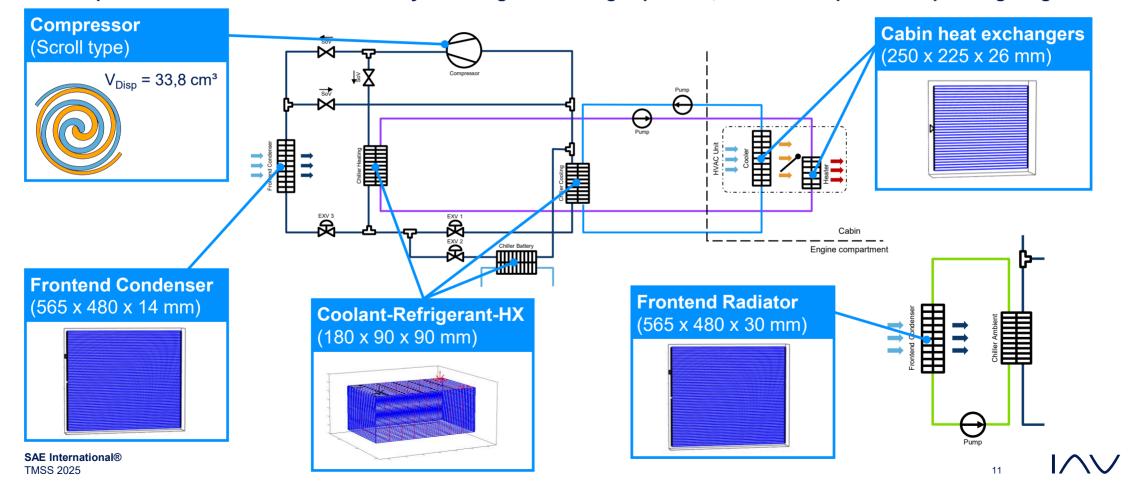
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Simulation Models

- Simulation of the whole system using geometrical and physical based simulation models
- Modeling of any component and connection to an overall system model
- Components were selected to meet today's heating and cooling capacities, installation space and operating range



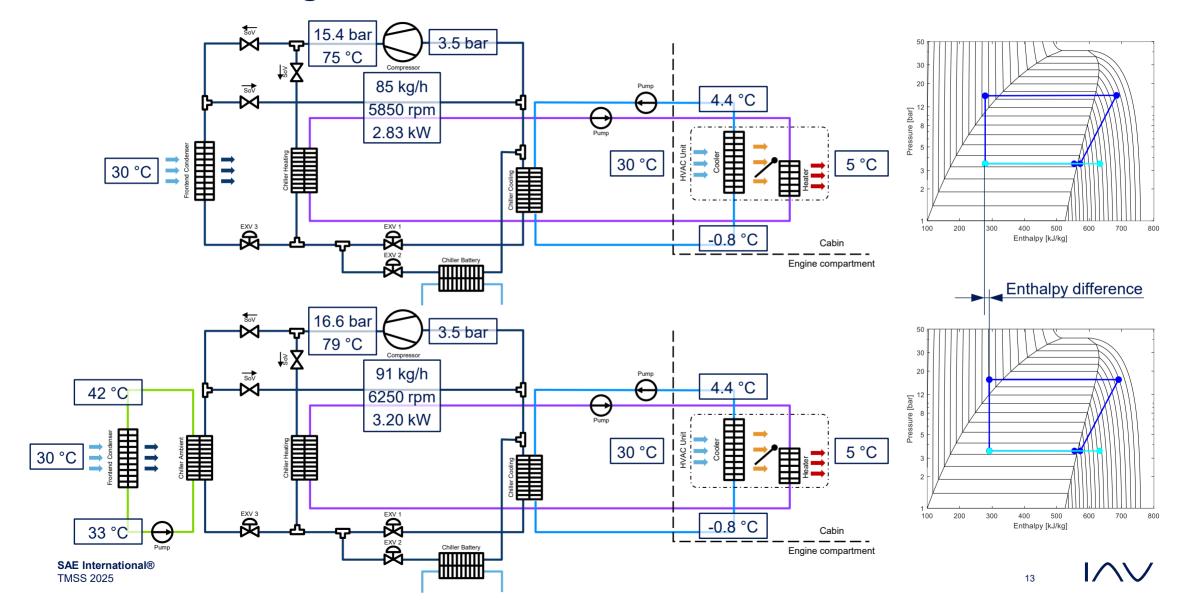
Boundary Conditions

• Simulations for typical summery conditions:

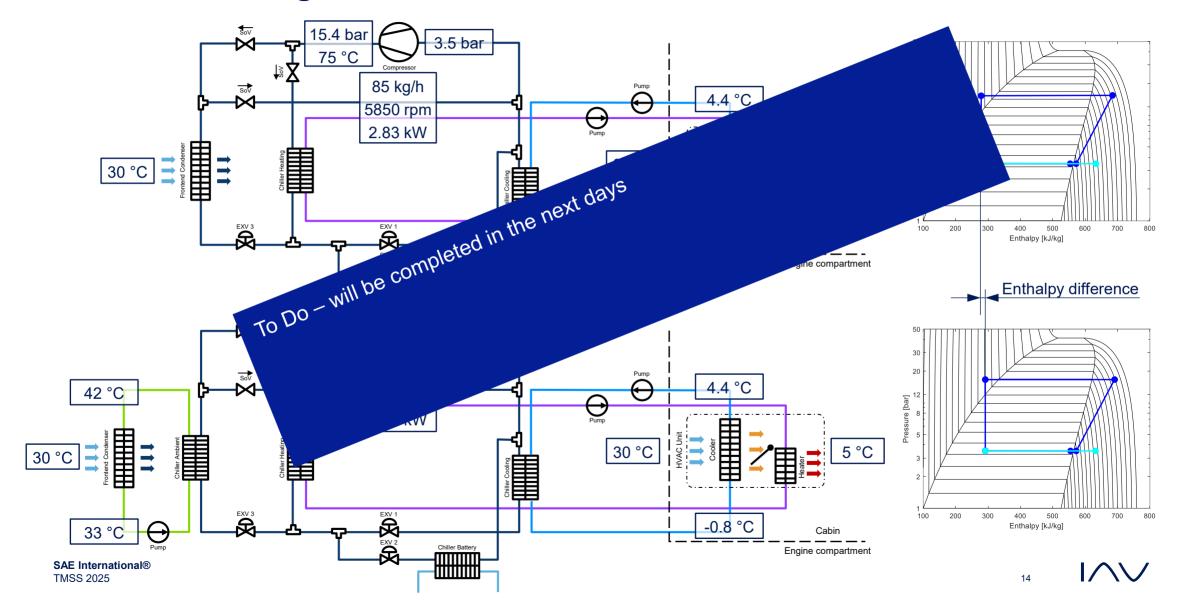
Parameter	Unit	1	II	III	IV	V	VI	VII	VIII
Ambient temperature	°C	20	25	30	32.5	35	0	-5	-10
Relative humidity	%	40							
Evaporator mass flow rate	kg/h	550							
Air temperature after Evaporator	°C	5					50		
Gas cooler air speed	m/s	4							

- Cooling capacities between 4.9 kW and 8.0 kW
- Coolant conditions at Chiller inlet: Ambient temperature, 10 L/min, 2 kW (Cooling mode)
- Tubes and hoses were not considered
- Fan powers were not considered either
- Refrigerant: R290 (Propane)

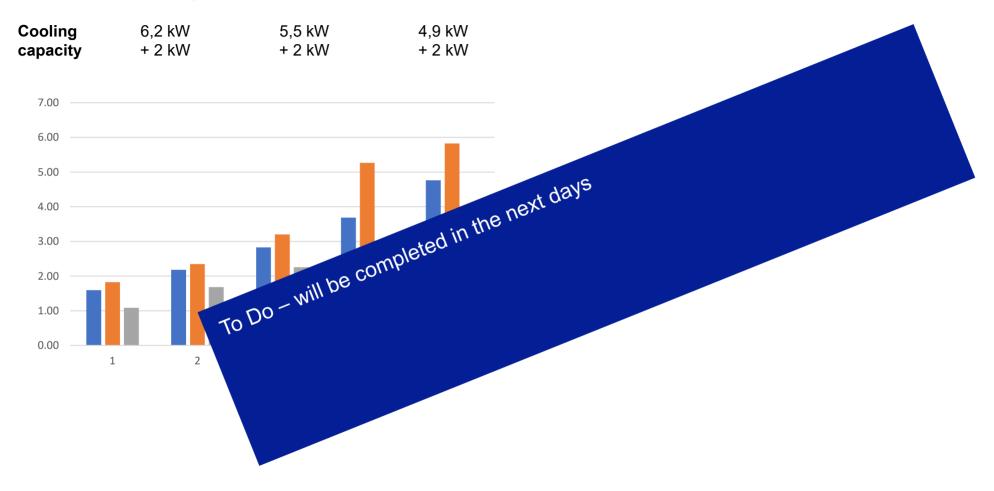
Results - Cooling mode at 30 °C



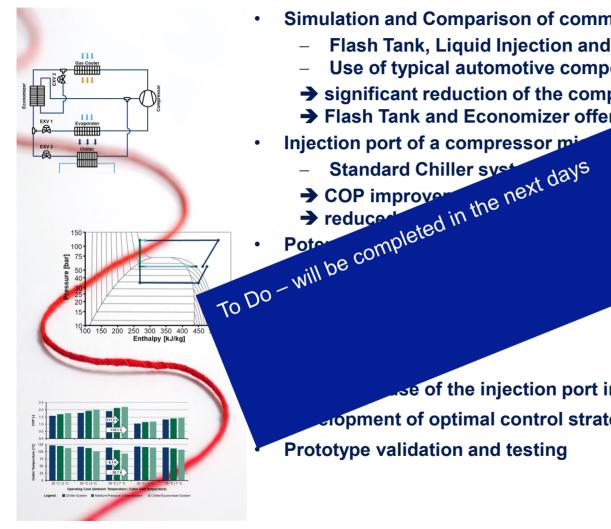
Results - Heating mode at -5 °C



Results – System comparison



Conclusion and Outlook



- **Simulation and Comparison of common injection systems:**
 - Flash Tank, Liquid Injection and Economizer
 - Use of typical automotive components and bound oday's electric cars
 - → significant reduction of the compressor
 - → Flash Tank and Economizer offers

oling power for fast charging

ortunities e.g., for direct evaporation battery w cell temperatures and a dew point dropping

- se of the injection port in heat pump operation propriet of optimal control strategies
- Prototype validation and testing

iller

mizer-system

Thank you!

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